Table VI. Comparison of Distillation Data for Separation of Trioxane and Solvent^b

particulars	dichlorobenzene	benzene
important solvent properties		
boiling point, °C	172-179	80.1
specific gravity, d_{4}^{20}	1.299	0.879
change in enthalpy $(H_T -$	5963 at	996 0
H_{200}), kcal/kg-mol	114.5	at 80
	°C (1)	°C (g)
toxicity (allowable limit),	<i>o</i> -, 50	
ppm	p-, 75	10
wt % trioxane in distillate	99.9	99.9
or bottom product		
min reflux ratio	0.5	1.0
operating reflux ratio	1.0	1.5
no. of theoretical stages	11.8	24.9
condenser duty, ^a kcal/h	2200	4700
reboiler duty, ^a kcal/h	2500	49 00

^a Calculated for processing extract, containing 10 kg/h trioxane. ^b Trioxane bp 114.5 °C.

aldehyde and water contents being higher, the operating costs for purification of trioxane to bring it to the monomer grade would be more.

Finally, trioxane has to be separated from the extracts by distillation. The data for the distillation from the extracts obtained at a solvent-to-feed ratio of 1.0 at 50 °C were calculated and are given in Table VI. The boiling points of benzene, o-dichlorobenzene, and trioxane are 80.1, 179, and 114.5 °C, respectively. Therefore, in the case of benzene extract, benzene would be the overhead product (at 80 °C) whereas, from the dichlorobenzene extract, trioxane would be distilled over at 114.5 °C. But in the former case the entire quantity of the benzene has to be separated by rectification. This would require a higher number of theoretical stages as well as operation at a higher reflux ratio. The consumption of energy will thus be higher. For the recovery of trioxane from dichlorobenzene extract, the requirements of theoretical stages, operating reflux, and heat load would be considerably lower. Moreover, benzene is more toxic than dichlorobenzene, and the allowable limits are 10 and 50 ppm, respectively (16). Hence, the expenses for safety precautions would be higher for benzene.

Glossary

solute
plait point
solvent
formaldehyde solution
weight fraction of solvent in solvent layer
weight fraction of formaldehyde solution in aqueous

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Heat Capacity and Enthalpy of Phosphoric Acid

Basil B. Luff

Division of Chemical Development, National Fertilizer Development Center, Tennessee Valley Authority, Muscle Shoals, Alabama 35660

Measurements of the heat capacity of phosphoric acid were made over the ranges of concentration of 61.8-83.0% and temperature of 25-367 °C. A possible transition was found at \sim 77 °C. Values for enthalpy were derived.

Previous studies (1) of the enthalpies of phosphoric acids and the derived heat capacities were made by using a high-temperature drop calorimeter. This study, using a Perkin-Elmer differential scanning calorimeter Model DSC-2, more precisely defines the heat capacities and entropies of the acids over a somewhat broader concentration range (61.8-83.0% P2O5) and temperature range (25-370 °C).

Materials and Procedure

The most concentrated superphosphoric acid (83.0% P₂O₅) was prepared by dissolving reagent P2O5 in reagent H3PO4 at

145 °C and filtering the hot solution through a coarse glass frit. Portions of this acid were diluted with reagent H₃PO₄ to form acids of the desired concentrations. All the solutions were held overnight at 100 °C to ensure equilibrium distribution of the phosphate species. Final concentrations of the acids were determined by chemical analyses.

The acid samples (17.56-29.87 mg) and a synthetic sapphire reference standard (40.09 mg) were hermetically sealed in weighed gold pans. The sample enclosure of the scanning calorimeter was cooled by an aluminum cold finger partially immersed in ice water and was purged continuously with dry nitrogen. The scanning rate for all measurements was 10 deg/min, and the sensitivity of the recorder was 2 mcal s⁻¹.

A weighed empty pan was placed in the sample holder and scanned over the desired temperature range. The empty pan was replaced with the pan containing the sapphire, and it was scanned over the same temperature range. The pan containing the sapphire was then replaced with the pan containing the acid

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Table I. Observed Heat Capacities of Phosphoric Acids

	61.8% P ₂ O ₅		$67.0\% P_2O_5$		$70.6\% P_2O_5$		72.6% P ₂ O ₅		74.1%	P ₂ O ₅	78.0%	P ₂ O ₅	83.0% P ₂ O ₅	
<i>Т</i> , К	C _s , cal K ⁻¹ g ⁻¹	SDª	$\overline{C_s}$, cal K ⁻¹ g ⁻¹	SDª	$\overline{C_{\mathbf{s}}, \operatorname{cal}}$ K ⁻¹ g ⁻¹	SDª	$\overline{C_{\rm s}}$, cal ${\rm K}^{-1} {\rm g}^{-1}$	SDª	$C_{\rm s}$, cal K ⁻¹ g ⁻¹	SDª	$C_{\mathbf{s}}$, cal K ⁻¹ g ⁻¹	SD ^a	C _s , cal K ⁻¹ g ⁻¹	SD ^a
300	0.4507	0.0006	0.4218	0.0006	0.3883	0.0003	0.3783	0.0007	0.3675	0.0004	0.3607	0.0004	0.3250	0.0005
310	0.4584	0.0004	0.4276	0.0003	0.3916	0.0006	0.3811	0.0008	0.3740	0.0004	0.3642	0.0007	0.3286	0.0003
320	0.4617	0.0004	0.4308	0.0004	0.3948	0.0002	0.3855	0.0005	0.3791	0.0004	0.3694	0.0012	0.3324	0.0003
330	0.4668	0.0010	0.4352	0.0002	0.3980	0.0004	0.3890	0.0007	0.3831	0.0003	0.3746	0.0014	0.3354	0.0004
340	0.4710	0.0005	0.4394	0.0003	0.4018	0.0007	0.3933	0.0007	0.3889	0.0005	0.3783	0.0013	0.3382	0.0006
350	0.4751	0.0008	0.4434	0.0004	0.4074	0.0012	0.3976	0.0009	0.3954	0.0002	0.3828	0.0014	0.3417	0.0010
360	0.4799	0.0011	0.4485	0.0008	0.4116	0.0014	0.4050	0.0012	0.4014	0.0003	0.3867	0.0016	0.3446	0.0011
370	0.4844	0.0016	0.4532	0.0012	0.4178	0.0022	0.4124	0.0013	0.4102	0.0002	0.3906	0.0014	0.3476	0.0013
380	0.4892	0.0017	0.4586	0.0013	0.4252	0.0028	0.4233	0.0020	0.4192	0.0004	0.3943	0.0018	0.3506	0.0015
390	0.4950	0.0017	0.4645	0.0011	0.4363	0.0033	0.4388	0.0029	0.4290	0.0002	0.3973	0.0019	0.3534	0.0018
400	0.4990	0.0014	0.4694	0.0008	0.4444	0.0033	0.4520	0.0036	0.4331	0.0001	0.4005	0.0022	0.3559	0.0021
410	0.5027	0.0015	0.4728	0.0005	0.4448	0.0024	0.4540	0.0014	0.4326	0.0005	0.4036	0.0021	0.3388	0.0023
420	0.5068	0.0018	0.4/69	0.0006	0.4432	0.0016	0.4485	0.0027	0.4350	0.0005	0.4068	0.0023	0.3011	0.0025
430			0.4808	0.0003	0.4442	0.0008	0.4480	0.0014	0.4380	0.0007	0.4093	0.0020	0.3037	0.0027
440			0.4830	0.0002	0.4470	0.0008	0.4309	0.0017	0.4419	0.0008	0.4117	0.0030	0.3000	0.0029
430			0.4090	0.0006	0.4529	0.0008	0.4333	0.0018	0.4434	0.0010	0.4141	0.0032	0.3081	0.0023
400					0.4538	0.0009	0.4500	0.0018	0.4511	0.0010	0.4195	0.0033	0.3707	0.0032
480					0.4608	0.0003	0.4634	0.0013	0.4536	0.0012	0.4113	0.0033	0.3750	0.0034
400					0.4000	0.0005	0.4657	0.0017	0.4552	0.0010	0.4276	0.00000	0.3766	0.0034
500							0.4681	0.0017	0.4571	0.0011	0.4220	0.0033	0.3786	0.0033
510							0.4001	0.0014	0.4586	0.0011	0.4240	0.0034	0.3700	0.0033
520							0.4735	0.0012	0.4603	0.0010	0 4274	0.0033	0.3823	0.0031
530							0.4754	0.0012	0.4610	0.0005	0.4286	0.0033	0.3838	0.0031
540							0.1701	0.0011	0.4628	0.0005	0.4296	0.0033	0.3850	0.0029
550									00=0	0.0000	0.4305	0.0034	0.3866	0.0028
560											0.4315	0.0035	0.3882	0.0027
570											0.4332	0.0030	0.3903	0.0024
580											0.4338	0.0033	0.3919	0.0021
590											0.4356	0.0029	0.3936	0.0018
600											0.4376	0.0026	0.3956	0.0015
610											0.4396	0.0025	0.3980	0.0012
620											0.4415	0.0024	0.4004	0.0008
630											0.4436	0.0020	0.4025	0.0004
640											0.4468	0.0021	0.4056	0.0005

^a SD = standard deviation.

and the scan repeated. The acid sample then was cooled as quickly as possible to the starting temperature and rescanned. The entire procedure was repeated several times for each acid sample, allowing at least 24 h between replicates. The pans containing the acid samples were weighed periodically to ascertain that no weight loss occurred during the measurements.

The heat capacities of the acids were determined at even temperature intervals by comparison of the ordinate displacement of the recording of the sample with that of the sapphire, the heat capacity of which is well-known (2), according to eq 1, where $C_a(S) =$ observed heat capacity of acid (cal deg⁻¹ g⁻¹),

$$C_{\rm s}(\rm S) = (\rm WR/WS)[(\rm DS - \rm DE)/(\rm DR - \rm DE)]C_{\rm p}(\rm R) \qquad (1)$$

 $C_p(R)$ = heat capacity of sapphire (cal deg⁻¹ g⁻¹), WS = weight of acid sample (mg), WR = weight of sapphire (mg), DS = ordinate displacement of pan plus acid (% of full scale), DR = ordinate displacement of pan plus sapphire (% of full scale), and DE = ordinate displacement of empty pan (% of full scale). Corrections based on the differences in weight between the empty pan and the sample pans and the heat capacity of gold were applied.

Heat Capacity and Enthalpy

The average observed heat capacities under the equilibrium vapor pressures, C_s , at even increments of absolute temperature along with their standard deviations are listed in Table I. An anomaly in the heat-capacity curves, possibly indicating a pronounced redistribution of phosphate species, was observed in the acids of lower concentration (61.8–74.1% P_2O_5) starting at ~350 K. The anomaly was rather small with the two acids

Table II. Enthalpies of Transition of Phosphoric Acids at 350 K

concn, % P ₂ O ₅	$\Delta H_{\mathrm{TR}},$ cal g ⁻¹	
61.8	0.004	
67.0	0.111	
70.6	0.974	
72.6	1.740	
74.1	0.692	

of lowest concentration (61.8-67.0% P2O5), and no significant differences could be detected between the first scan and the scan immediately after cooling, indicating that equilibrium at the starting temperature was attained guickly upon cooling. The average observed heat capacities for these acids were obtained from all of the scans. The anomaly was more pronounced with three of the acids (70.6, 72.6, and 74.1% P2O5), and significant differences could be detected in the anomaly between the first scan and the scan immediately after cooling, indicating that, although the acids were converting back to the low-temperature form, equilibrium had not been attained. The heat capacities for these acids at temperatures below and above the anomaly showed no significant differences between the first and second scan; so for these acids, all of the observed heat capacities at temperatures below and above the anomaly were used to determine the average values. Only those from the first scans were used for the average values in the anomaly. The anomaly was not observed in the heat-capacity curves of the two acids of highest concentration (78.0 and 83.0% P2O5), and no significant differences could be detected between the first and second scans; so for these acids, all of the observed heat capacities were used to determine the average values. Poly-

	% P205	$(H_T - H_{2,2}).$	cal g ⁻¹	0.000	3.874	10.513	17.279	ion	17.279	24.169	31.178	38.300	45.527	52.851	60.264	67.758	75.326	82.963	90.666	98.436	106.275	114.190	122.193
	83.09	C cal	deg ^{~1} g ⁻¹	0.325	0.329	0.335	0.341	no transit	0.341	0.348	0.353	0.359	0.364	0.368	0.373	0.377	0.380	0.384	0.387	0.390	0.394	0.398	0.403
	6 P205	$(H_T - H_{22})$.	cal g ⁻¹	0.000	4.295	11.684	19.246	ion	19.246	26.972	34.850	42.867	51.006	59.254	67.593	76.010	84.493	93.032	101.621	110.258	118.948	127.699	136.529
	78.09	C. ट्वा	deg ⁻¹ g ⁻¹	0.360	0.365	0.374	0.382	no transit	0.382	0.390	0.397	0.404	0.410	0.415	0.419	0.423	0.426	0.428	0.431	0.433	0.436	0.439	0.444
	P205	$H_T - H_{aa.}$	cal g ⁻¹	0.000	4.391	11.965	19.741	0.692	20.433	28.627	37.011	45.566	54.275	63.118	72.079	81.137	90.276	99.477					
	74.1%	C _s , cal	deg ⁻¹ g ⁻¹	0.368	0.374	0.384	0.394		0.405	0.415	0.424	0.432	0.439	0.445	0.451	0.455	0.459	0.461					
	.6% P ₂ O ₅	$(H_T - H_{298}),$	cal g ⁻¹	0.000	4.491	12.197	20.063	1.740	21.803	30.371	39.051	47.844	56.749	65.768	74.899	84.144	93.501	102.971					
	72.1	$C_{\rm s}, {\rm cal}$	deg ⁻¹ g ⁻¹	0.377	0.381	0.389	0.397		0.426	0.431	0.437	0.442	0.448	0.454	0.459	0.465	0.471	0.476					
Acids	P205	$(H_T - H_{298}),$	cal g ⁻¹	0.000	4.616	12.514	20.547	0.974	21.521	29.939	38.488	47.169	55.981	64.925	74.000								
hosphoric /	70.6%	C _s , cal	deg ⁻¹ g ⁻¹	0.388	0.392	0.398	0.405		0.418	0.424	0.431	0.437	0.444	0.450	0.457								
298.15 K of P	% P ₂ O ₅	$(H_T - H_{29h})$	cal g ⁻¹	0.000	5.026	13.643	22.430	0.111	22.541	31.611	40.838	50.221	59.760	69.455									
ange above	67.0	$C_{\rm s}, {\rm cal}$	$deg^{-1} g^{-1}$	0.422	0.427	0.435	0.444		0.450	0.457	0.465	0.473	0.481	0.489									
Enthalpy Char	% P ₁ O5	$(H_T - H_{29,8}),$	cal g ⁻¹	0.000	5.386	14.623	24.044	0.004	24.048	33.680	43.481	53.453											
Capacity an	61.8	C _s , cal	deg ⁻¹ g ⁻¹	0.452	0.457	0.466	0.476	lg⁺¹	0.477	0.486	0.494	0.503											
Table III. Heat		temp,	K	298.15	310	330	350	ΔH_{TR} , ca	350	370	390	410	430	450	470	490	510	530	550	570	590	610	630



Figure 1. Enthalpy of transition of phosphoric acids.



Figure 2. Enthalpy change above 25 °C for phosphoric acids.

nomial equations of the heat capacity as a function of temperature were fitted to the observed values below and above the anomaly. The enthalpies of transition, $\Delta H_{\rm TR}$, in cal g⁻¹ were determined from eq 2. The first term on the right side of eq

$$\Delta H_{\rm TR} = \int_{350}^{T} (C_{\rm s})_{\rm a} \, \mathrm{d}T - \int_{350}^{T} (C_{\rm s})_{\rm f} \, \mathrm{d}T \qquad (2)$$

Table IV. Heat Capacity of Phosphoric Acid, cal g^{-1} °C⁻¹

τ°0	P205,	62	64	66	£9	70	72	74	76	79	80	83
<u> </u>	WL 70	02		00	00		12	/4	/0	/0	00	02
25		0.450	0.441	0.429	0.414	0.395	0.380	0.368	0.365	0.360	0.351	0.337
40		0.457	0.448	0.436	0.420	0.400	0.386	0.376	0.372	0.366	0.358	0.343
50		0.462	0.452	0.440	0.424	0.403	0.390	0.381	0.376	0.371	0.362	0.346
60		0.467	0.457	0.444	0.428	0.407	0.393	0.386	0.381	0.375	0.366	0.350
70		0.471	0.461	0.448	0.432	0.410	0.397	0.391	0.386	0.379	0.369	0.353
80		0.478	0.469	0.458	0.444	0.426	0.424	0.407	0.392	0.384	0.373	0.356
90		0.482	0.473	0.462	0.448	0.429	0.427	0.412	0.397	0.388	0.376	0.359
100		0.486	0.477	0.466	0.451	0.432	0.430	0.416	0.402	0.391	0.379	0.361
110		0.491	0.481	0.470	0.455	0.436	0.433	0.421	0.406	0.395	0.382	0.364
120		0.495	0.486	0.474	0.459	0.439	0.436	0.425	0.411	0.399	0.385	0.366
130		0.499	0.490	0.478	0.462	0.442	0.439	0.429	0.415	0.402	0.387	0.369
140		0.504	0.494	0.482	0.466	0.446	0.442	0.433	0.419	0.405	0.390	0.371
150		0.508	0.498	0.486	0.469	0.449	0.445	0.437	0.422	0.408	0.392	0.373
160			0.503	0.490	0.473	0.452	0.448	0.441	0.426	0.411	0.394	0.375
170				0.494	0.477	0.456	0.451	0.444	0.429	0.413	0.396	0.377
180					0.480	0.459	0.454	0.447	0.432	0.416	0.398	0.379
190					0.484	0.462	0.457	0.450	0.434	0.418	0.400	0.381
200						0.465	0.460	0.453	0.437	0.420	0.401	0.383
210						0.469	0.463	0.456	0.439	0.421	0.403	0.384
220							0.466	0.459	0.441	0.423	0.405	0.386
230							0.469	0.461	0.442	0.425	0.406	0.388
240								0.464	0.443	0.426	0.408	0.390
250								0.466	0.445	0.427	0.409	0.391
260								0.468	0.445	0.429	0.411	0.393
270									0.446	0.430	0.412	0.395
280									0.446	0.431	0.414	0.396
290									0.446	0.432	0.415	0.398
300									0.446	0.434	0.417	0.400
310									0.446	0.435	0.419	0.401
320										0.436	0.420	0.403
330										0.438	0.422	0.405
340										0.440	0.424	0.407
350										0.442	0.426	0.409
360										0.445	0.428	0.411
370										0.448	0.430	0.413

Table V. Enthalpy of Phosphoric Acid, $H_T - H_{25}$, cal g⁻¹

	P ₂ O ₅ ,	()	()		(0)	70	70	74	76	70	90	0.7
<i>T, 'C</i>	wt %	62	64	00	68	/0	12	/4	/0	/8		82
40		6.8	6.7	6.5	6.3	6.0	5.7	5.6	5.5	5.4	5.3	5.1
50		11.4	11.2	10.9	10.5	10.0	9.6	9.4	9.3	9.1	8.9	8.5
60		16.1	15.7	15.3	14.7	14.0	13.5	13.2	13.1	12.9	12.6	12.0
70		20.7	20,3	19.7	19.0	18.1	17.5	17.1	16.9	16.6	16.2	15.5
80		25.5	25.0	24.3	23.6	23.0	23.2	21.8	20.9	20.5	19.9	19.1
90		30.3	29.7	28.9	28.1	27.2	27.5	25.9	24.9	24.3	23.7	22.6
100		35.1	34.4	33.6	32.6	31.5	31.8	30.1	28.9	28.2	27.5	26.2
110		40.0	39.2	38.3	37.1	35.9	36.1	34.2	32.9	32.1	31.3	29.9
120		44.9	44.1	43.0	41.7	40.3	40.4	38.5	37.0	36.1	35.1	33.5
130		49.9	48.9	47.7	46.3	44.7	44.8	42.7	41.1	40.1	39.0	37.2
140		54.9	53.9	52.5	50.9	49.1	49.2	47.0	45.3	44.1	42.8	40.9
150		60.0	58.8	57.4	55.6	53.6	53.6	51.4	49.5	48.2	46.8	44.6
160			63.8	62.2	60.3	58.1	58.1	55.8	53.7	52.3	50.7	48.4
170				67.2	65.1	62.6	62.6	60.2	58.0	56.4	54.6	52.1
180					69.9	67.2	67.1	64.7	62.3	60.6	58.6	55.9
190					7 4 .7	71.8	71.7	69.2	66.6	64.7	62.6	59.7
200						/6.4	76.3	73.7	/1.0	68.9	00.0	63.5
210						81.1	80.9	/8.2	/3.4	73.1	70.0	07.4
220							83.3	02.0	/9.0	91 6	79.7	75.1
230							90.2	07.4	04.2 99 2	01.0	10.1	79.0
240								92.0	03.0	00.0	86.0	82.0
250								101.3	97.5	90.1	91.0	86.8
200								101.5	101.9	98 7	95 1	90.7
280									106.4	103.0	99.2	94.7
290									110.9	107.3	103.4	98.6
300									115.3	111.6	107.5	102.6
310									119.8	116.0	111.7	106.6
320										120.3	115.9	110.7
330										124.7	120.1	114.7
340										129.1	124.3	118.8
350										133.5	128.6	122.9
360										137.9	132.9	127.0
370										142.4	137.1	131.1

2 was determined by tabular integration of the average observed heat capacities as a function of temperature in the anomaly, and the last term was determined by integrating the heat capacity equation above the anomaly over the temperature range of the tabular integration. The values for the enthalpy of transition calculated in this manner are listed in Table II and shown in Figure 1.

Values for heat capacity and enthalpy change above 298.15 K at even intervals of temperature for the phosphoric acids were calculated from the heat-capacity equations, their integrals with the proper integration constants, and the heats of transition listed in Table II. These values are listed in Table III. Enthalpy changes above 298.15 K also were calculated at the same temperatures as those reported by Wakefield et al. (1), and the values compared in Figure 2. The results are in good agreement except at 72.6% P2O5, a concentration in which the enthalpy of transition is quite pronounced, and above 350 K (77 °C), the temperature of the transition. This discrepancy probably can be explained by the fact that only the energy released as the acid cools from the higher temperature to 298.15 K in a short period of time would be measured by the drop calorimeter. The slow release of energy as the acid converts from the high-temperature form to the low-temperature form, which takes several hours, would not be detected.

Values of heat capacity of the phosphoric acid calculated from the heat-capacity equations were plotted against concentration at each 10-degree interval of temperature, and smooth curves were drawn through the points. Values of heat capacity at each 10-degree interval of temperature for phosphoric acids at even intervals of concentration then were read from the curves. Values of the enthalpy of transition at even intervals of concentration were read from Figure 1. Equations were fitted to these values, and the heat capacities and enthalpy changes above 298.15 K were determined as described above and are listed in Tables IV and V, respectively. The temperatures were converted to Celsius to make the report compatible with the previous one (1).

Corrections for converting C_s to C_p , the heat capacity at constant pressure, based on vapor pressures and enthalpies of vaporization taken from the literature (3) and the assumption that the liquids occupied 75% of the encapsulated volumes were less than 0.001 cal deg⁻¹ g⁻¹ over most of the temperature ranges but did increase to 0.002 cal deg⁻¹ g⁻¹ when the liquids were near their boiling points. These corrections, approximately the same magnitude as the differences between the observed and calculated heat capacities, were considered to be within the precision of the measurements.

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Solubility of Acetone and Isopropyl Ether in Compressed Nitrogen, Methane, and Carbon Dioxide

Paul J. Hicks, Jr., and John M. Prausnitz*

Chemical Engineering Department, University of California, Berkeley, California 94720

Vapor-phase solubilities are reported for acetone and isopropyl ether in compressed nitrogen, methane, and carbon dioxide, in the range -50 to 50 °C and 17-63 bar. The experimental solubilities are reduced to obtain second virial cross-coefficients. Experimental cross-coefficients are compared to those calculated by using the square-well potential or the Hayden-O'Connell correlation.

There is little fundamental information concerning the interaction between a small nonpolar molecule (2) and a large polar molecule (1). To obtain such information, it is useful to measure the second virial cross-coefficient B_{12} which is directly related to the intermolecular potential Γ_{12} . This work reports experimental measurements which yield B_{12} for a number of binary polar-nonpolar mixtures. The experimental data obtained are the solubilities of acetone and isopropyl ether in compressed nitrogen, methane, and carbon dioxide.

These measurements are also of interest in chemical engineering because they provide the fundamental information needed to calculate solvent losses in an absorption process operating at advanced pressure.

This work is similar to that of Lazaide et al. (1), who studied the solubility of methanol in compressed gases.

Experimental Section

The experimental apparatus is similar to that used by Lazakle (1). There are some minor modifications made primarily to

facilitate changing pressures in the apparatus. A schematic of the flow apparatus is shown in Figure 1.

A light (gaseous) component is equilibrated with a heavy (liquid) component at a given temperature and pressure. The gas phase is sampled and analyzed.

The light component is fed from a gas cylinder through a pressure regulator and a precooling/preheating coil to the two equilibrium cells arranged in series. The gas enters the bottom of each equilibrium cell, containing the liquid being studied, through a stainless-steel sparger whose average pore size is 5 μ m. The slowly flowing gas is saturated with the liquid as it bubbles through the liquid. Two cells in series are used to ensure that the exiting gas is nequilibrium with the liquid. The top of each cell is packed with glass wool to remove any possible entrainment of the liquid in the gas. The gas exits the second cell through a section of tubing heated to prevent condensation of the heavy component. In this section the gas is expanded to atmospheric pressure. The volumetric flow rate is always less than 0.3 cm³/s where the measured solubility is independent of the flow rate.

The constant-temperature bath containing the equilibrium cells is controlled by a Hallikainen (Shell Development) thermotrol to ± 0.05 °C or better except at -50 °C where it is controlled to ± 0.15 °C or better. At low temperatures, the bath fluid is 95% ethanol; at high temperatures, it is water. Temperatures above -10 °C are measured with a set of liquid-inglass calorimetric thermometers with an accuracy of ± 0.1 °C. Temperatures between -10 and -25 °C are measured with a